

「高度DFC-  
PowerChipに向けたレーザー描画の開発(項目⑦⑱)」

> 40 MW unstable cavity microchip laser for laser writing

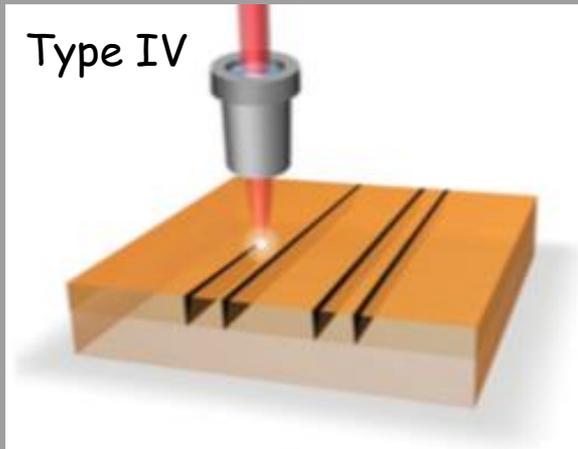
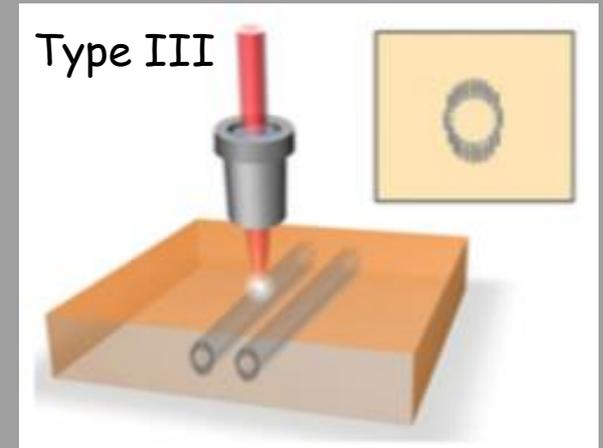
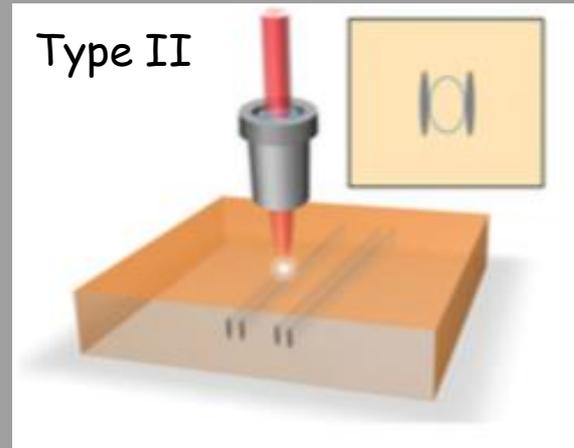
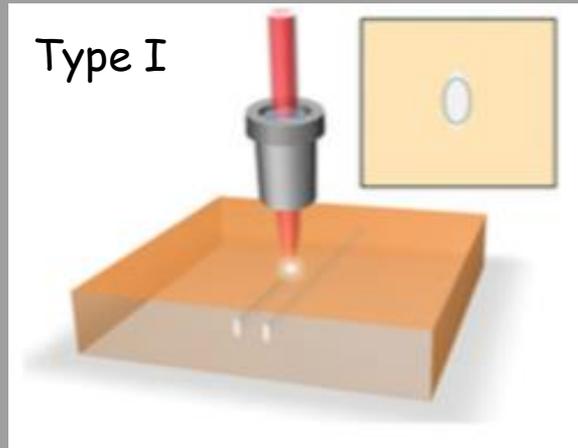
**Hwan Hong LIM**

*Division of Research Innovation and Collaboration  
Institute for Molecular Science (IMS)*

# Outline

1. Overview of fs-laser micromachined waveguide
2. Record peak power microchip laser with unstable cavity
3. Summary

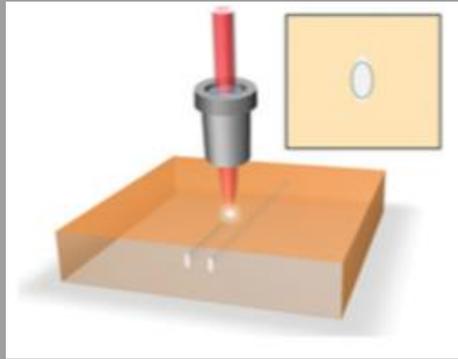
# fs-laser micromachined waveguides



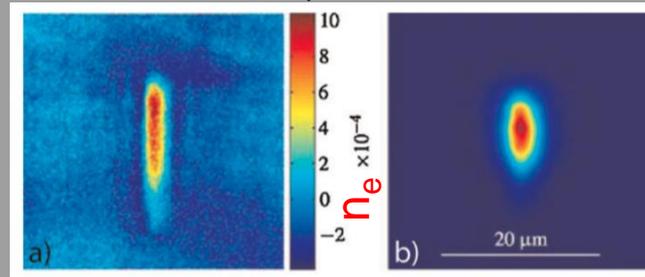
- Mechanism:
  - Strong field ionization (MPI, TI)
  - a hot and dense electronic plasma, and a lattice of ions
  - Ultra fast ablation by Coulomb explosion (electrons and ions ejection)
- Laser parameters ( $w_0$ ,  $\tau$ ,  $E$ ,  $f$ )
- Material properties ( $E_g$ ,  $W$ ,  $\kappa$ , GVD)

Ref. F. Chen and J. R. Vazquez de Aldana, Laser Photonics Rev. **8**, 251-275 (2014).

# Type I : Directly written waveguides



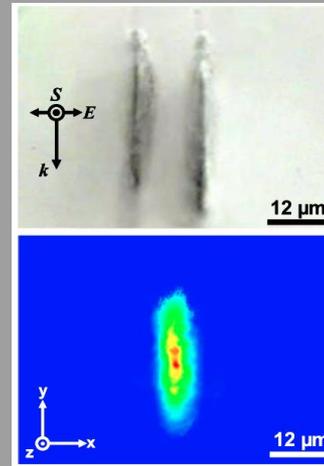
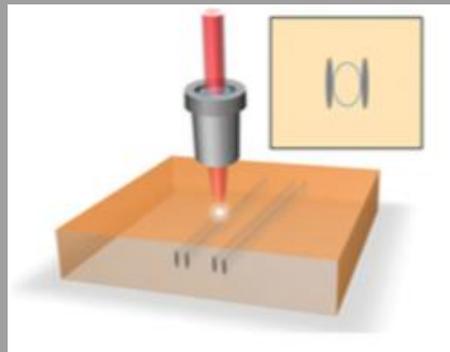
LN,  $\sim 0.2 \mu\text{J}$ ,  $\sim 100 \text{ fs}$



Appl. Phys. A 89, 127 (2007).

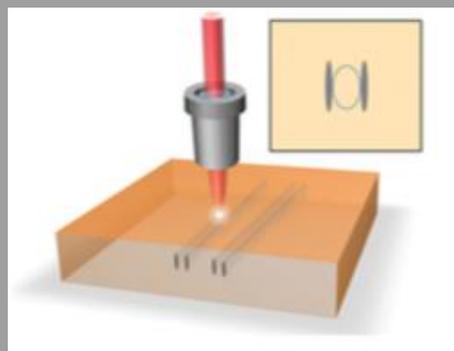
- ◆  $\Delta n > 0$  in the focal volume  $\rightarrow$  the waveguide core
  - Positive change is very common in amorphous materials, e.g., in most glasses.
  - A few crystals (LN, Nd:YCOB and ZnSe) were used for Type I waveguide.
- ◆ Weak damage or modification
  - Point defect creation for LN  $\rightarrow$  lower spontaneous polarization
- ◆ Advantages
  - Ease 3D fabrication
- ◆ Disadvantages
  - Degradation of bulk related properties in the core due to the even weak damage (NLO coefficient, PL, ...)
  - Unstable or removed under high temperature, not suitable for high-power applications
  - Light polarization sensitive guiding

# Type II : Stress induced waveguides

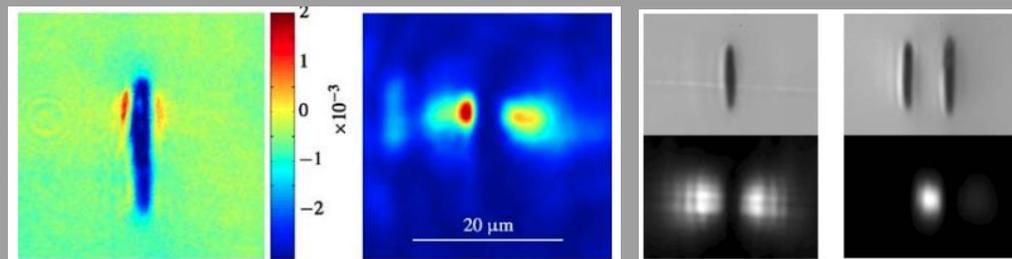


- ◆ The waveguides are in the vicinal region of the fs-laser induced tracks.
- ◆  $\Delta n < 0$  in the focal volume due to expansion of the lattices  $\rightarrow$  a relatively high index in the vicinal surrounding regions by stress-induced effects.
- ◆ Advantages
  - Preservation of luminescence and nonlinear properties of the bulk.
  - Both TM, TE guiding is possible in some crystals.
  - Very stable waveguide at high temperature, suitable for high power operation.

# Type II : Stress induced waveguides

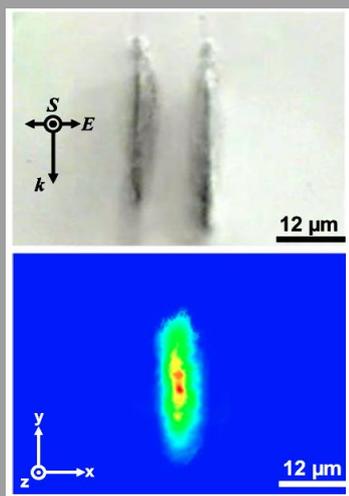


x-cut LN,  $\sim 0.3 \mu\text{J}$ ,  $\sim 1.2 \text{ ps}$ , 100 kHz, 1 mm/s.



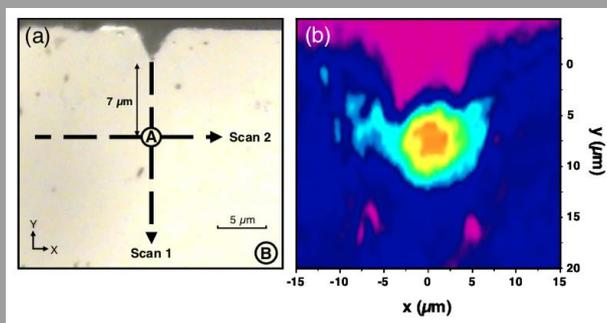
Appl. Phys. A 89, 127 (2007).

Nd(2 at.):YAG ceramic  
(Baikowski Japan),  
 $\sim 0.8 \mu\text{J}$ ,  $\sim 120 \text{ fs}$ , 1 kHz, 50  $\mu\text{m/s}$ .



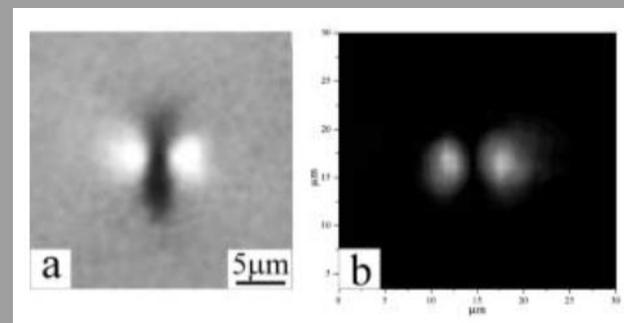
Appl. Phys. B 95, 85 (2009).

Nd(2 at.):YAG ceramic (Baikowski  
Japan),  
 $\sim 4 \text{ J/cm}^2$ ,  $\sim 120 \text{ fs}$ , 1 kHz, 25  $\mu\text{m/s}$ .



Opt. Express 15, 13266 (2007).

$\alpha$ -quartz ([001]//k),  
 $\sim 14 \mu\text{J}$ ,  $\sim 120 \text{ fs}$ , 1 kHz,  $< 1 \text{ mm/s}$ .

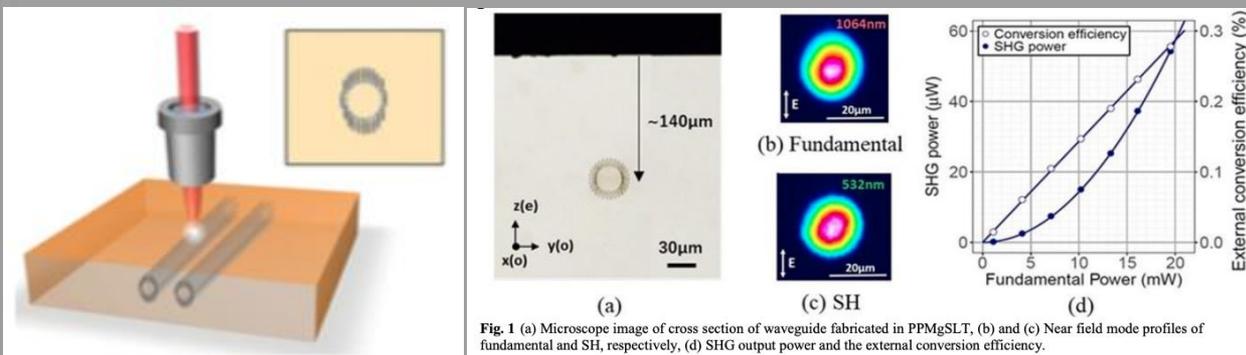


Appl. Phys. A 76, 309 (2003).

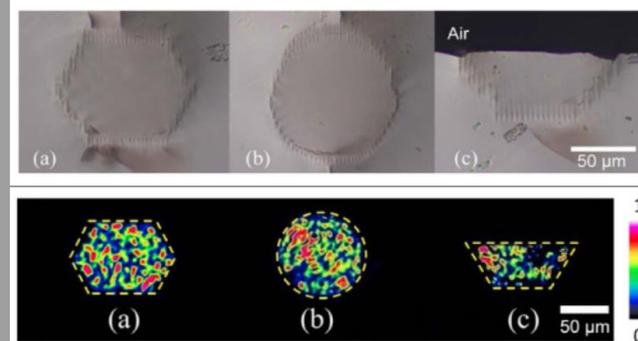
# Type III : Depressed cladding waveguides

PPMgSLT,  $\sim 0.4 \mu\text{J}$ , 300 fs

Nd:YAG ceramic,  $< 0.4 \mu\text{J}$ , 120 fs, 1 kHz, 0.7 mm/s



OXIDE Co. CLEO\_Europe (2019).



- ◆ Similar to Type II,  $\Delta n < 0$  in the focal volume. The waveguide consists of a core surrounded by a number of low-index tracks. Those tracks are close to each other (few micrometers), constructing a quasicontinuous low-index potential barrier wall, which allows the confinement of the light field inside.

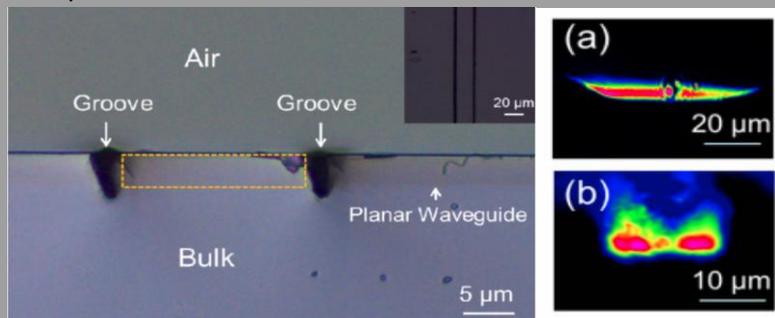
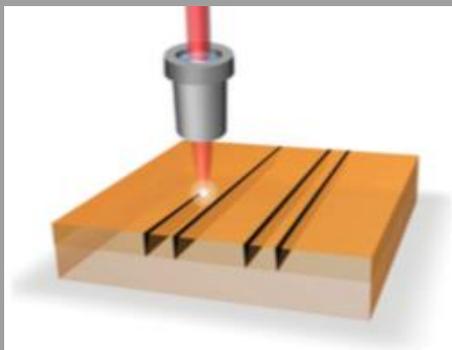
## ◆ Advantages

- Designable waveguide cross section shape and size.
- Circular cross section is suitable for fiber-waveguide-fiber integrated photonic system.

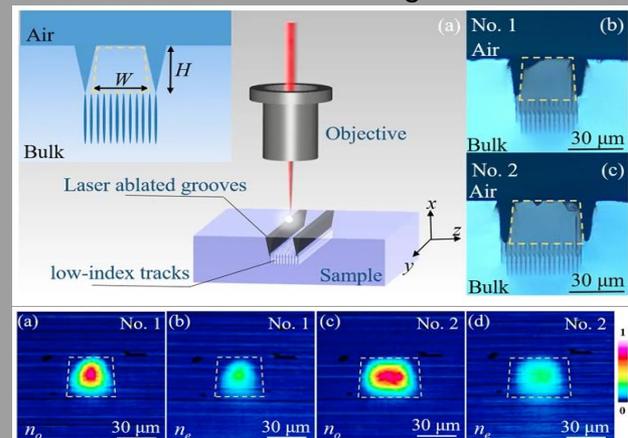
# Type IV : Ablated ridge waveguides

x-cut LiNbO<sub>3</sub>, <0.3 μJ, 120 fs, 1 kHz, 0.5 mm/s,  
for mid-IR wavelength

Nd:YAG crystal, 2.1 μJ, ~50 J/cm<sup>2</sup>, 120 fs, 1 kHz,  
50 μm/s



Opt. Mat. Express 2, 657 18620 (2012).

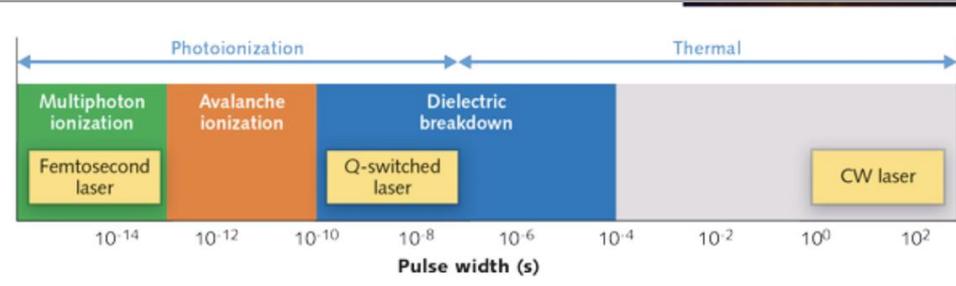


Sci. Rep. 7, 7034 18620 (2017).

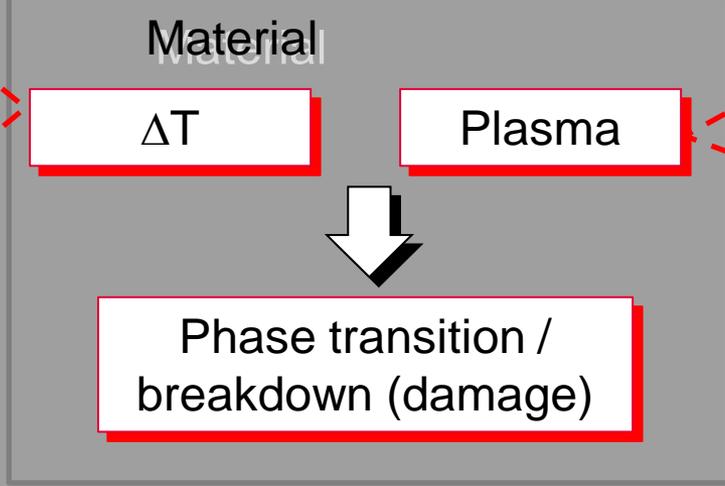
- ◆ High intensity fs pulse induced ablation.
- ◆ Construction of ridge waveguide on planar waveguide substrates.
- ◆ All laser machined ridge waveguide (Type III + IV).
- ◆ Disadvantage
  - ◆ Rough side wall by ablation (Loss of >> 3 dB/cm)
  - ◆ A postablation treatment such as ion-beam sputtering or HF etching may be required to reduce the roughness of the ablated air gaps.

# Pulse width dependence of laser induced breakdown

Laser  
( $\tau, \omega$ )

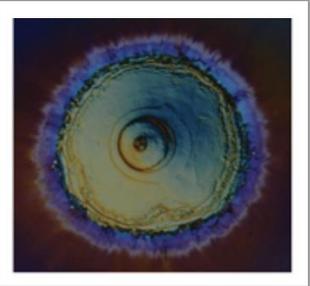


- Thermal explosion model
- Thermal lensing
- ...

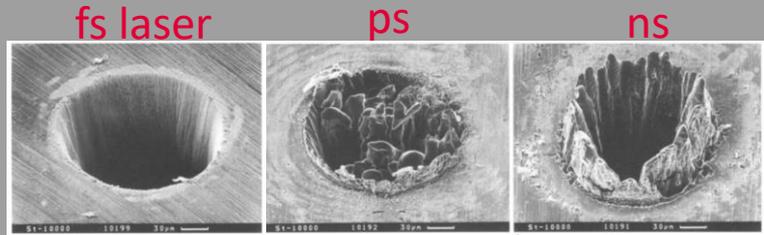


- Impact cascade (avalanche) ionization
- Photon ionization
- Kerr lensing for filamentation
- ...

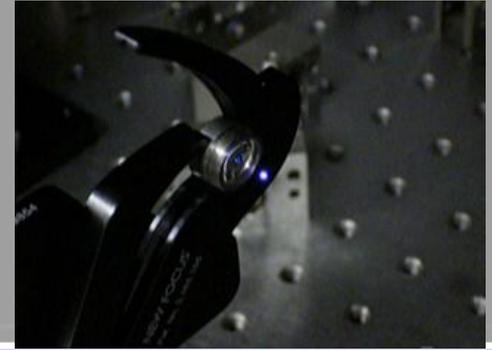
Damage on a dielectric coating



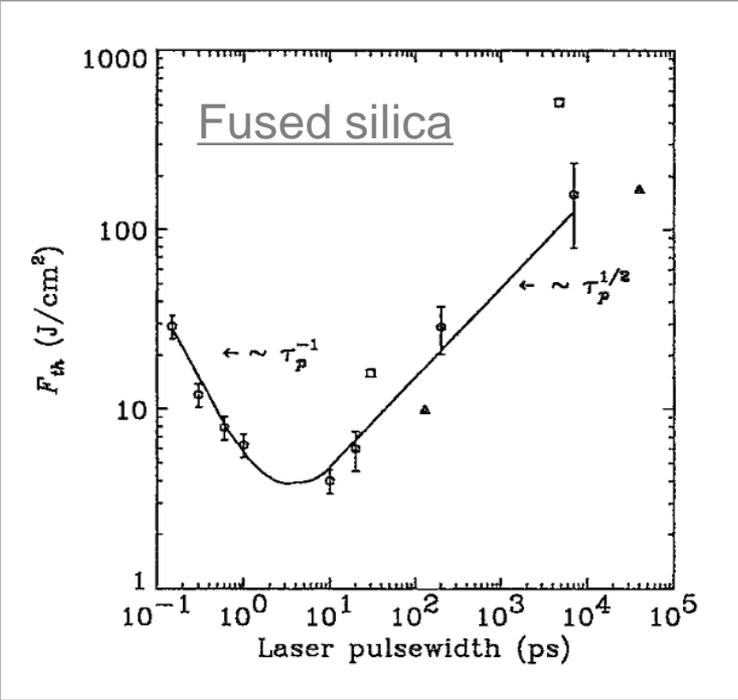
Drilling in steel foils



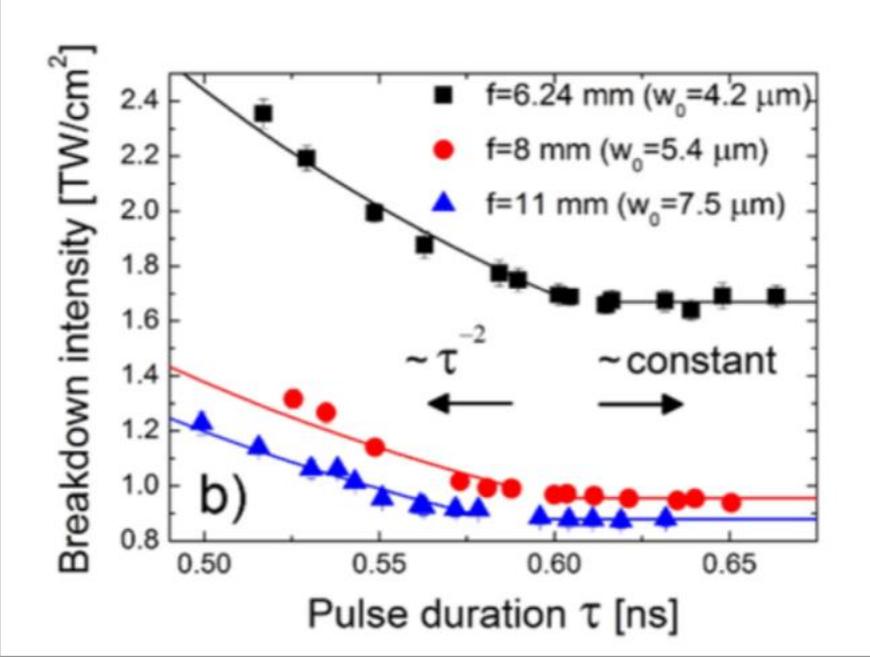
Gas-lighter ignition using laser induced air-breakdown spark



# Pulse width dependent breakdown threshold

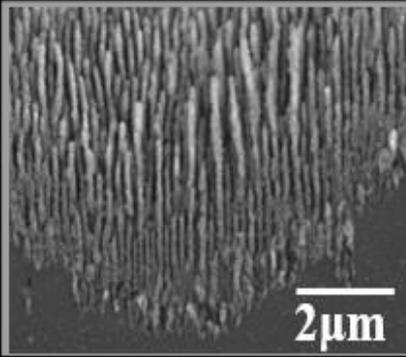
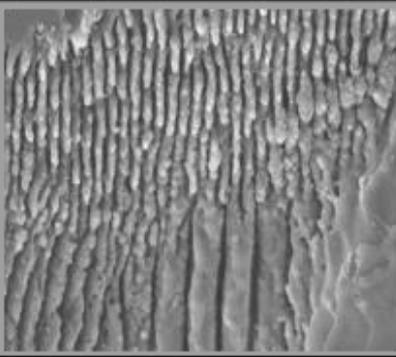
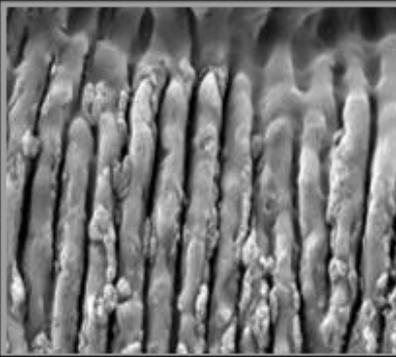
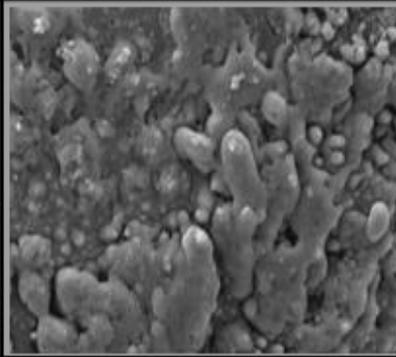


D. Du, et al., Appl. Phys. Lett. **64**, 3071 (1994).



H. H. Lim and T. Taira, Opt. Express **25**, 6302 (2017).

# Pulse width dependent laser-induced periodic surface structure (LIPSS)

(a) $T = 450$ fs	(b) $T = 500$ ps	(c) $T = 1$ ns	(d) $T = 2.5$ ns
$N = 1666$	$N = 500$		
$1 \mu\text{J}/\text{pulse}$	$1 \text{ mJ}/\text{pulse}$		
			
HSFL	HSFL and LSFL	LSFL	-



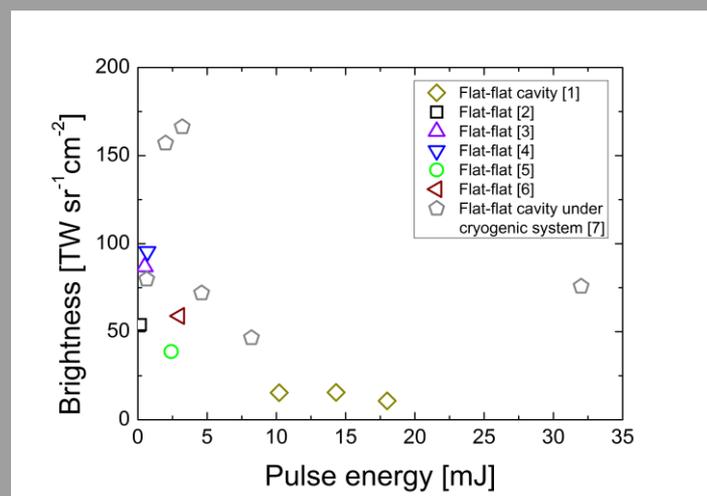
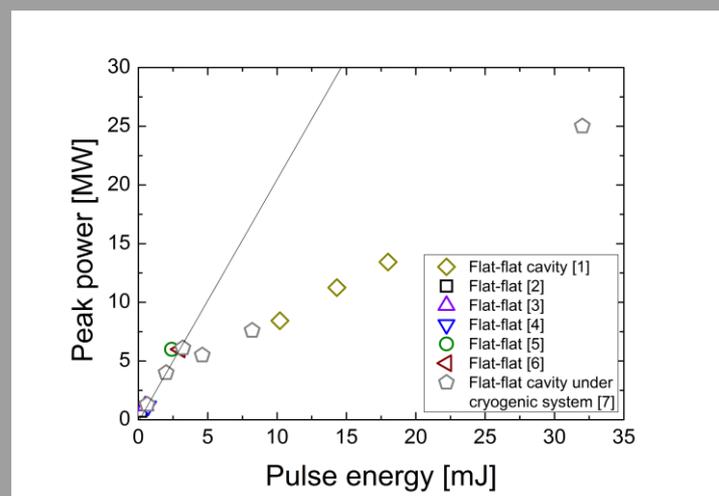
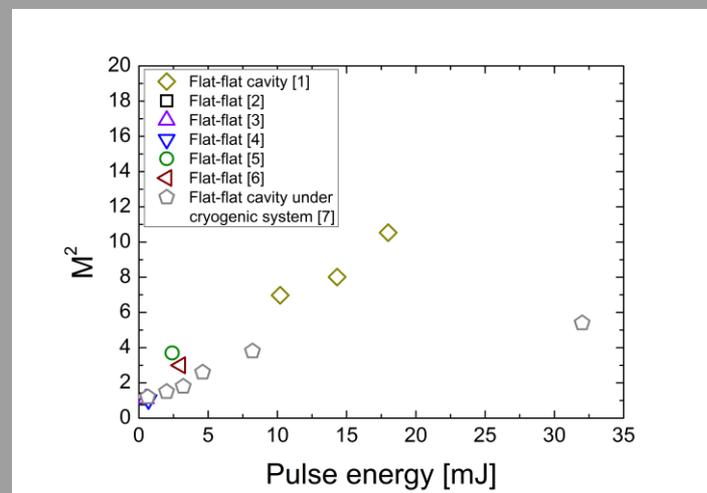
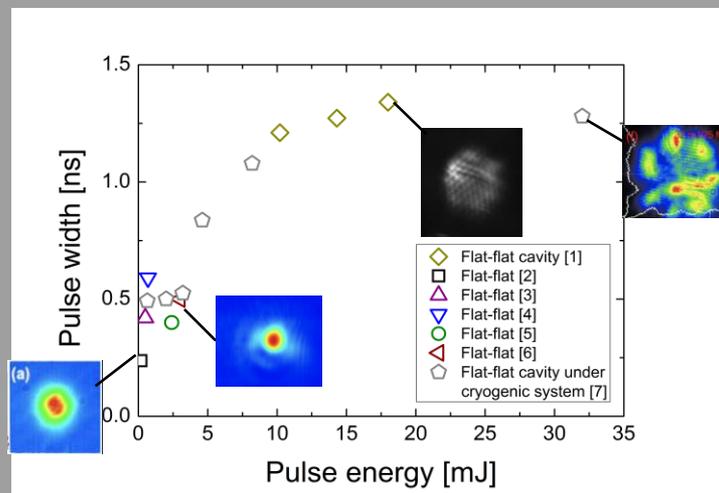
Surface SEM images of LIPSS on 6H-SiC.  $T =$  (a) 450 fs, (b) 500 ps, (c) 1 ns and (d) 2.5 ns

Ref. R. Miyagawa, T. Taira, et al., LIC 2019, LIC6-5.

# Outline

1. Overview of fs-laser micromachined waveguide
2. Record peak power microchip laser with unstable cavity
3. Summary

# Problems of brightness scale for flat-flat cavity MCL



[1] H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

[2] J. Dong, et al., Opt. Express **15**, 14516 (2007).

[3] A. Agnesi, et al., Appl. Phys. Lett. **89**, 101120 (2006).

[4] H. Sakai, T. Taira, et al., Opt. Express **16**, 19891 (2008).

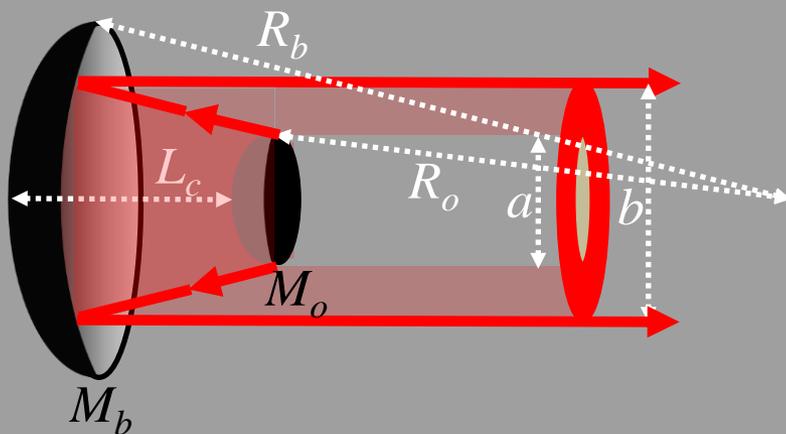
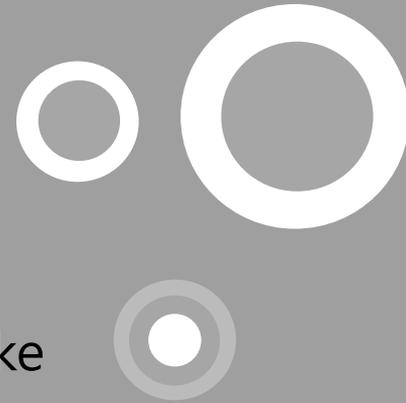
[5] N. Pavel, T. Taira, et al., Opt. Express **19**, 9378 (2011).

[6] H. H. Lim and T. Taira, Opt. Express **25**, 6302 (2017).

[7] X. Guo, et al., Opt. Express **27**, 45 (2019).

# Unstable cavity MCL for brightness scaling

- ▶ Wider and controllable mode volumes
- ▶ Uniform beam pattern of doughnut shape
  - ▶ No beam pattern degradation for energy scaling
- ▶ A good focusability of doughnut beam as a Bessel-like beam



$$m = \frac{b}{a} = -\frac{R_b}{R_o}$$

$$R_b = \frac{2mL_c}{m-1}$$

$$R_o = -\frac{2L_c}{m-1}$$



$$m = \sqrt{2}$$

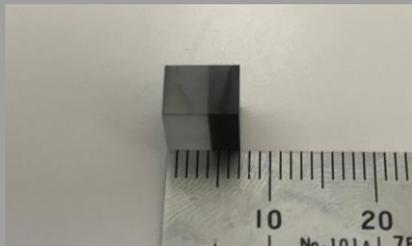
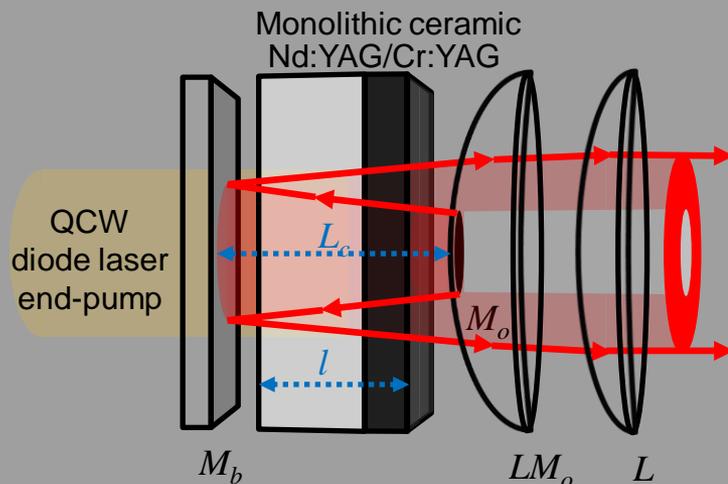
$$m = 2$$

$$m = 3$$

Positive branch confocal cavity

# Experimental setup I : flat-convex cavity

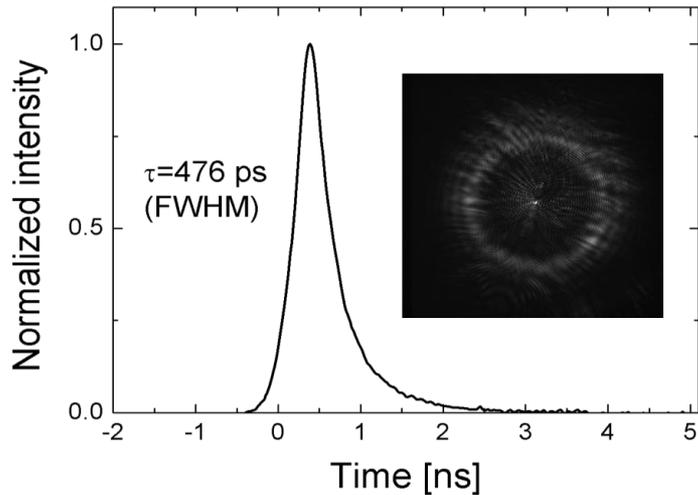
## Microchip laser with unstable cavity



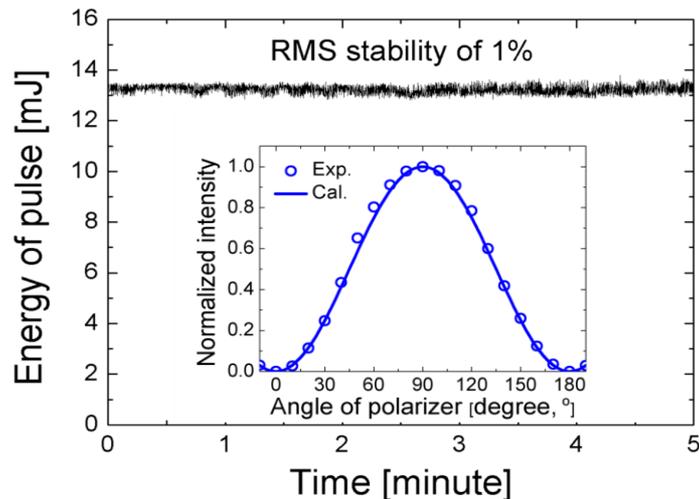
- ▶ 700 W pump diode @ 808 nm, 10 Hz during  $<400 \mu\text{s}$
- ▶ Monolithic ceramic with a dimension of 6 X 6 X 7( $l$ ) mm<sup>3</sup>
- ▶ 1.1 at.% Nd<sup>3+</sup> doping and 30% of initial transmittance of Cr<sup>4+</sup>:YAG
- ▶ Flat back cavity mirror  $M_b$
- ▶ A half inch plano-convex lens  $LM_o$  with a radius of curvature of 52 mm (for  $m$  of  $\sqrt{2}$  for the confocal cavity)
- ▶ Output coupler (OC)  $M_o$ , HR coated on the center part of  $LM_o$  in a spot diameter of 2 mm
- ▶ Collimation lens  $L$  with a focal length of 50~150 mm in case of the lens position

H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

# Laser characteristics

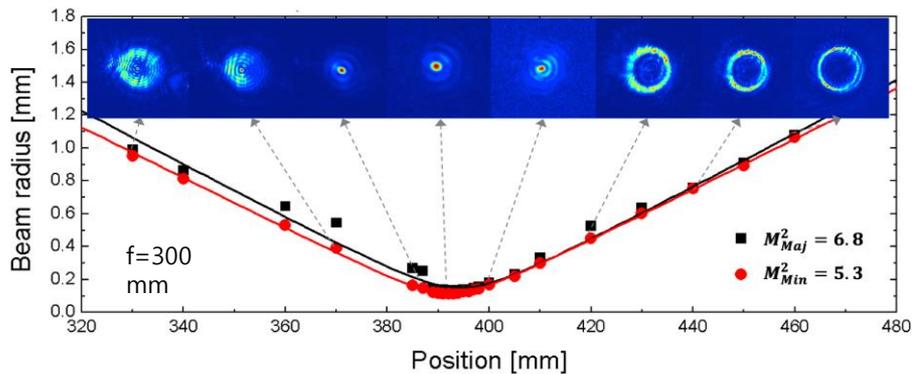


- ▶ Doughnut beam pattern with a center Poisson spot
- ▶ Pulse energy of 13.2 mJ @ 10 Hz
- ▶ Pulse width of 476 ps
  - ▶ Record peak power of 27.7 MW



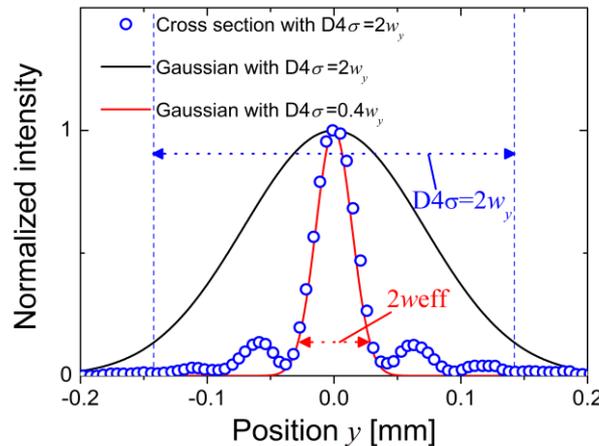
- ▶ Short term RMS stability <1%
- ▶ Linear polarization @ 10 Hz  
(may be pump power induced birefringence and depolarization due to stress and heat)
  - ▶ The polarization ratio  $P = \frac{I_{max} - I_{min}}{I_{max} + I_{min}} = 0.997$   
H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

# Beam quality and pattern



- ▶  $M^2 (M_{pc}^2) = 6 (5.8)$ , second-moment based  $M^2$  and 86.5% power-content based  $M_{pc}^2$
- $$M_{ave}^2 = \sqrt{M_{maj}^2 M_{min}^2}$$

- ▶ Bessel-like beam at focal point



- ▶ The center part (red line) of Bessel-like beam has 0.2 times smaller size than  $D4\sigma$  (black line).

- ▶ The small center part can increase focusability substantially.

$M_{eff}^2$ : effective  $M^2$

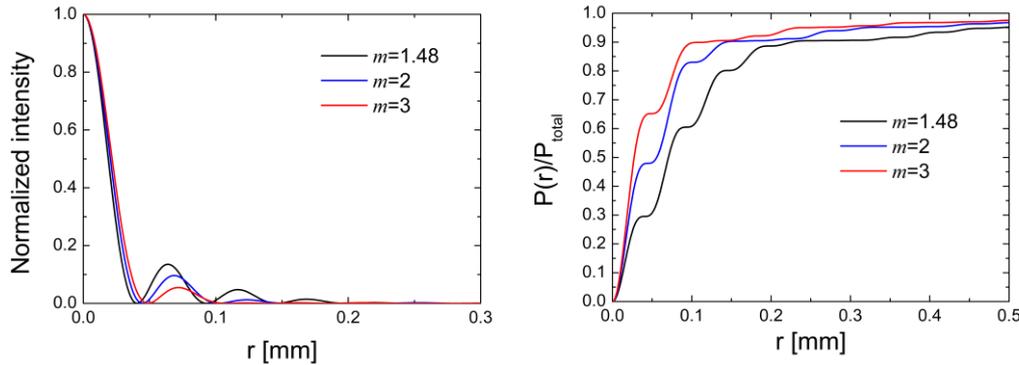
$w_{0,eff}$ : effective beam waist

$\theta$ : half angle divergence

$$M_{eff}^2 = \frac{\pi w_{0,eff}}{\lambda} \theta = \frac{\pi w_{0,eff}}{\lambda} \cdot \frac{\lambda M^2}{\pi w_0} = \frac{w_{0,eff}}{w_0} M^2 = 0.2 \times 6 = 1.2.$$

H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

# Laser characteristics around far-field



▶ The center part portion of pulse energy

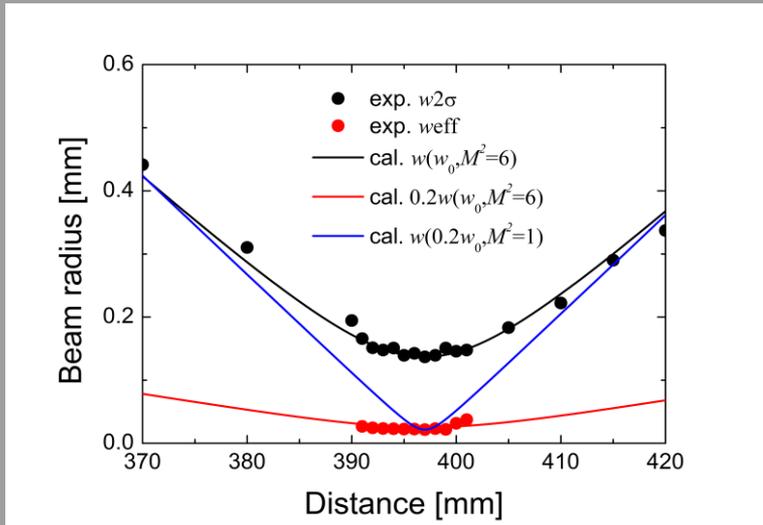
$$E_{eff} \approx 30\% \text{ for } m=1.48$$

$$E_{eff} \approx 65\% \text{ for } m=3$$

Intensity distribution of plane wave focused by an annular aperture at the focal plane

$$I(r, f) = \frac{4 I(0, f)}{(1 - 1/m^2)^2} \left[ \frac{J_1(kr b/f)}{kr b/f} - \frac{1}{m^2} \frac{J_1(kr a/f)}{kr a/f} \right]^2, \quad (1)$$

where  $m = b/a$  is the ratio of the outer radius  $b$  and the inner radius  $a$  of the aperture,  $S = \pi a^2(m^2 - 1)$  is the annular area,  $J_1$  is the first-order Bessel function,  $k = 2\pi/\lambda$  is the wave number,  $f$  is the focal length, and  $I(0, f) = S^2/(\lambda^2 f^2)$  is the peak intensity at the focal plane. [1] B. Lu, et al., J. Mod. Opt. **48**, 1171 (2001).



▶ The center part self-diffracts as the same as  $D4\sigma$

▶ The effective Rayleigh length of the center part is about 4 times longer than that of Gaussian

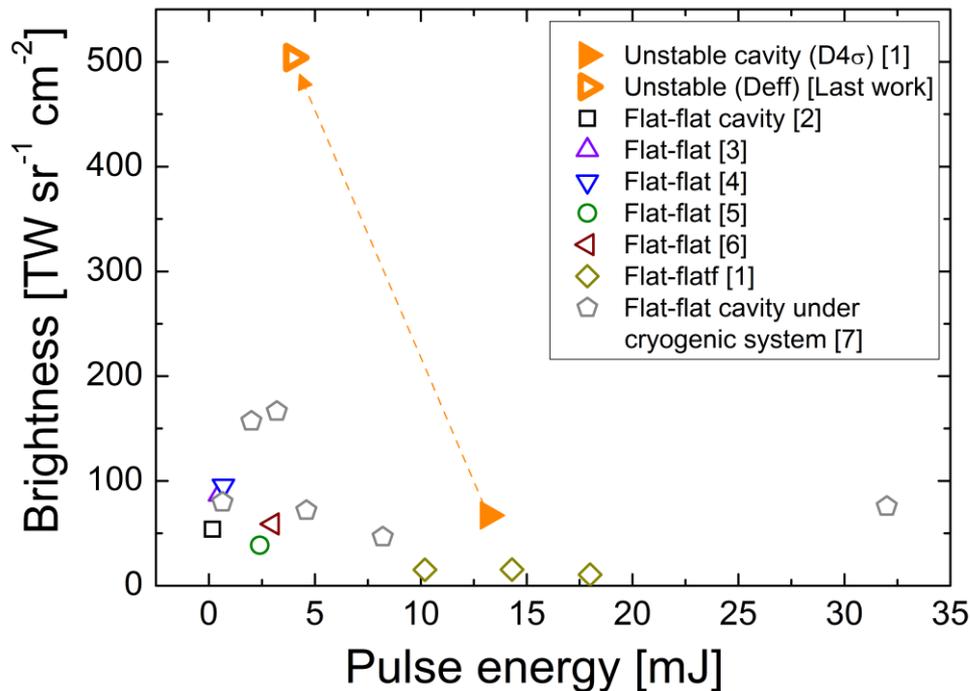
$$Z_{R,eff} \approx 4 \times Z_{R,G}(M^2=1)$$

(Red line)

(Blue line)

H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

# Compared brightness to other works



[1] H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

[2] J. Dong, et al., Opt. Express **15**, 14516 (2007).

[3] A. Agnesi, et al., Appl. Phys. Lett. **89**, 101120 (2006).

[4] H. Sakai, T. Taira, et al., Opt. Express **16**, 19891 (2008).

[5] N. Pavel, T. Taira, et al., Opt. Express **19**, 9378 (2011).

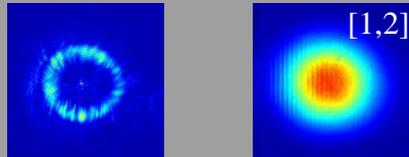
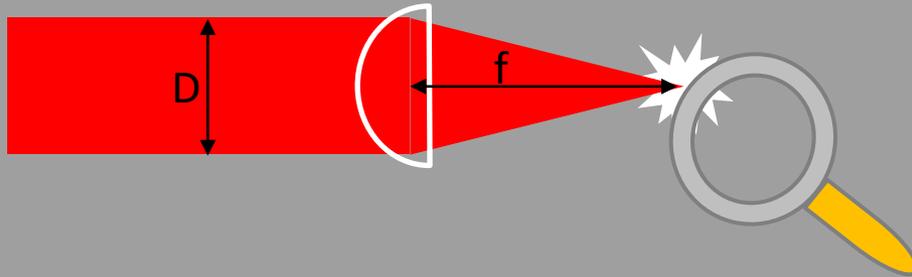
[6] H. H. Lim and T. Taira, Opt. Express **25**, 6302 (2017).

[7] X. Guo, et al., Opt. Express **27**, 45 (2019).

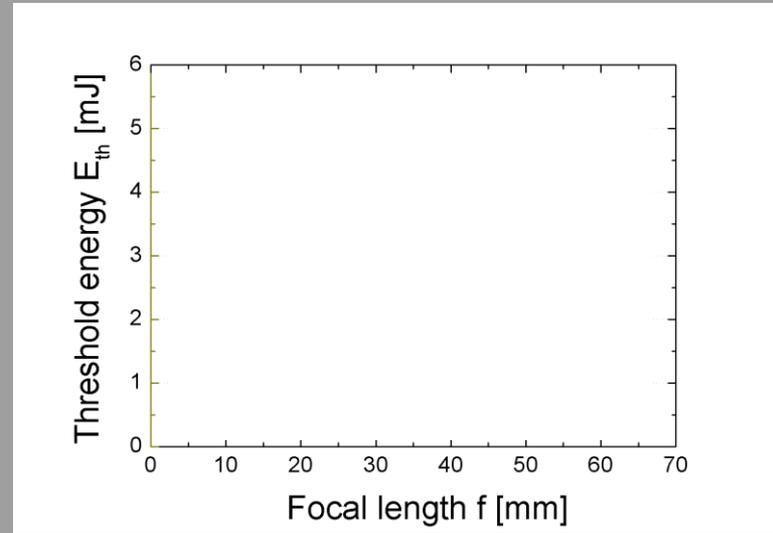
▶  $E_{eff} = 30\%$ ,  $M_{eff}^2 = 1.2$

▶ Highest effective brightness of over 0.5 PW sr<sup>1</sup> cm<sup>-2</sup>

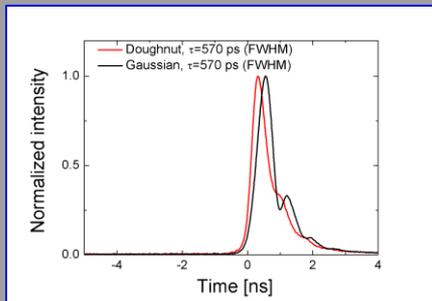
# Laser induced breakdown (LIB) in air



$D=7.5$  mm     $D=7.5$  mm  
 $\tau=0.57$  ns     $\tau=0.57$  ns  
 $M^2=5.1$          $M^2=1.3$



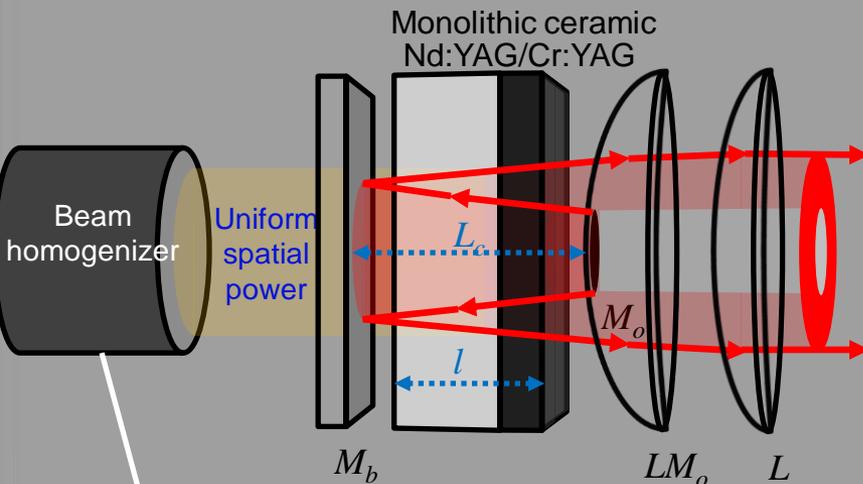
▶ Comparable capability of LIB to a near-Gaussian beam due to the effective high brightness of doughnut beam at focal plane



[1] H. H. Lim and T. Taira, Opt. Express **25**, 6320 (2017).

[2] H. H. Lim and T. Taira, Opt. Express **27**, 31307 (2019).

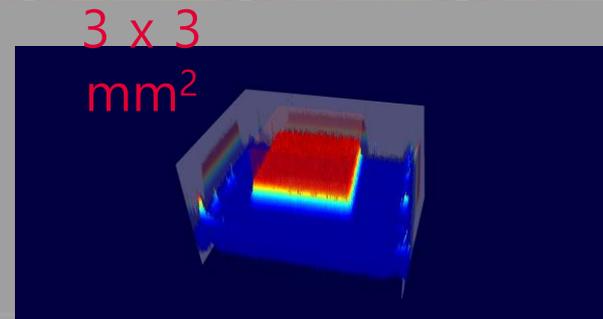
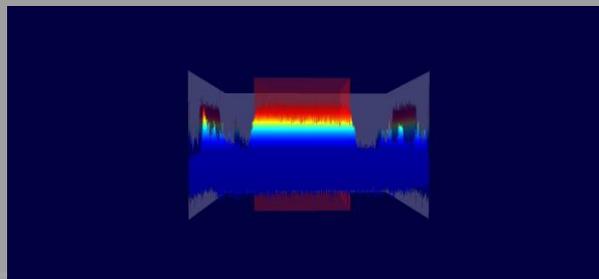
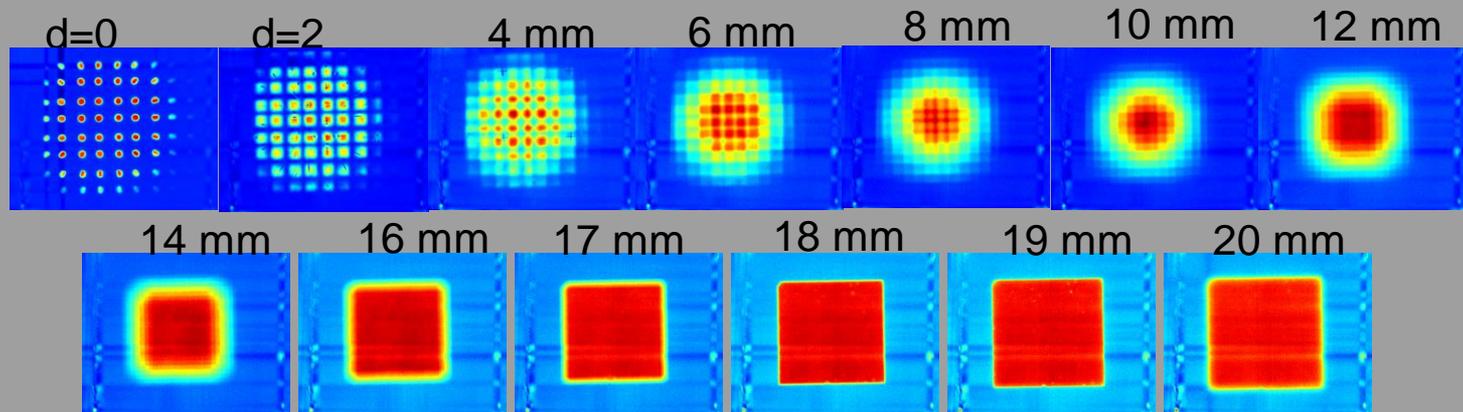
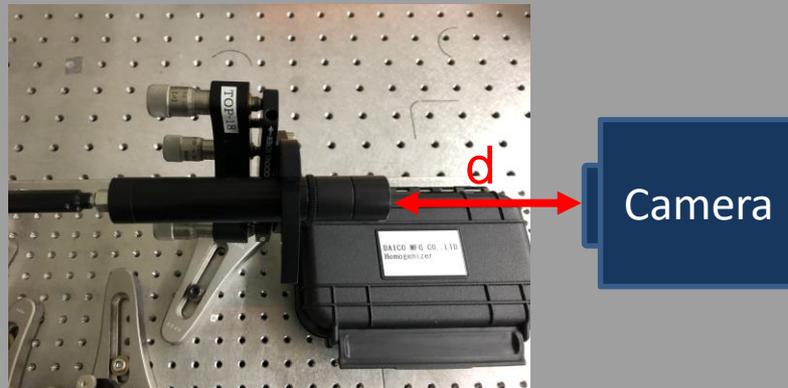
# Experimental setup II : flat-convex cavity & uniform pump-power distribution



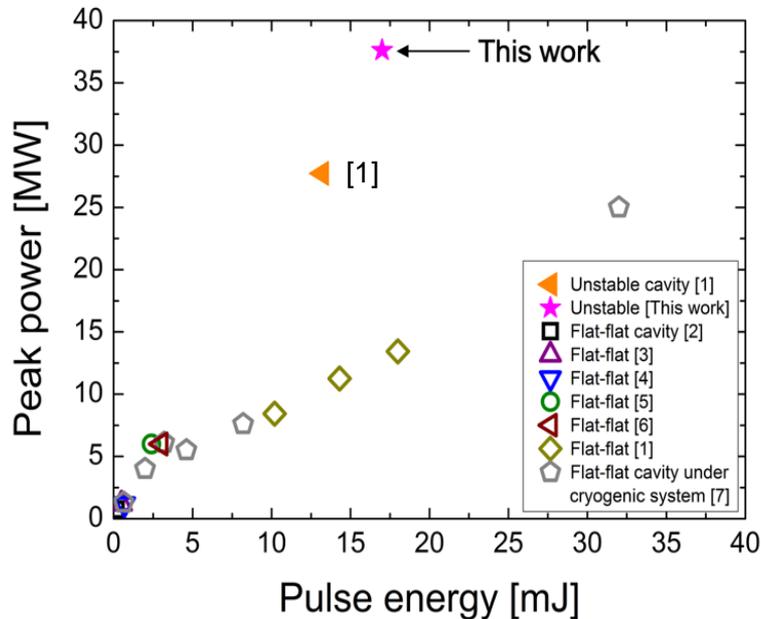
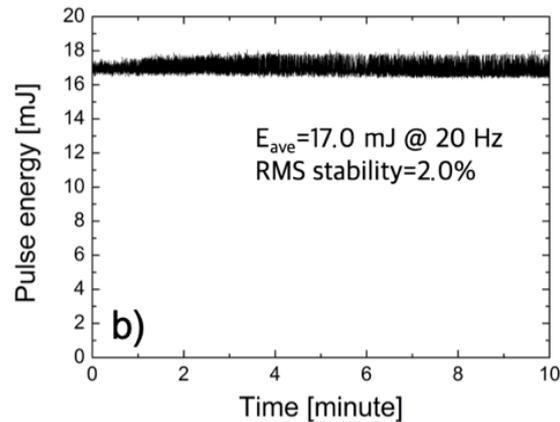
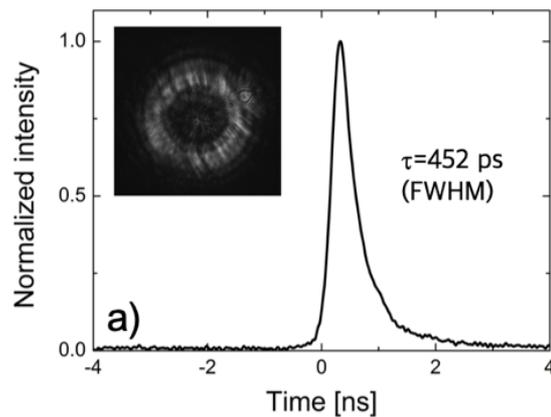
- ▶ 1.5 kW pump diode @ 808 nm, 20 Hz during <400  $\mu$ s
- ▶ Uniform pump power distribution:  $\sim 3 \times 3$  mm<sup>2</sup>
- ▶ Flat back cavity mirror  $M_b$
- ▶ A half inch plano-convex lens  $LM_o$  with a radius of curvature of 52 mm (for  $m$  of  $\sqrt{2}$  for the confocal cavity)
- ▶ Output coupler (OC)  $M_o$ , HR coated on the center part of  $LM_o$  in a spot diameter of 2 mm
- ▶ Collimation lens  $L$  with a focal length of 50~150 mm in case of the lens position



# Experimental setup II : flat-convex cavity & uniform pump-power distribution



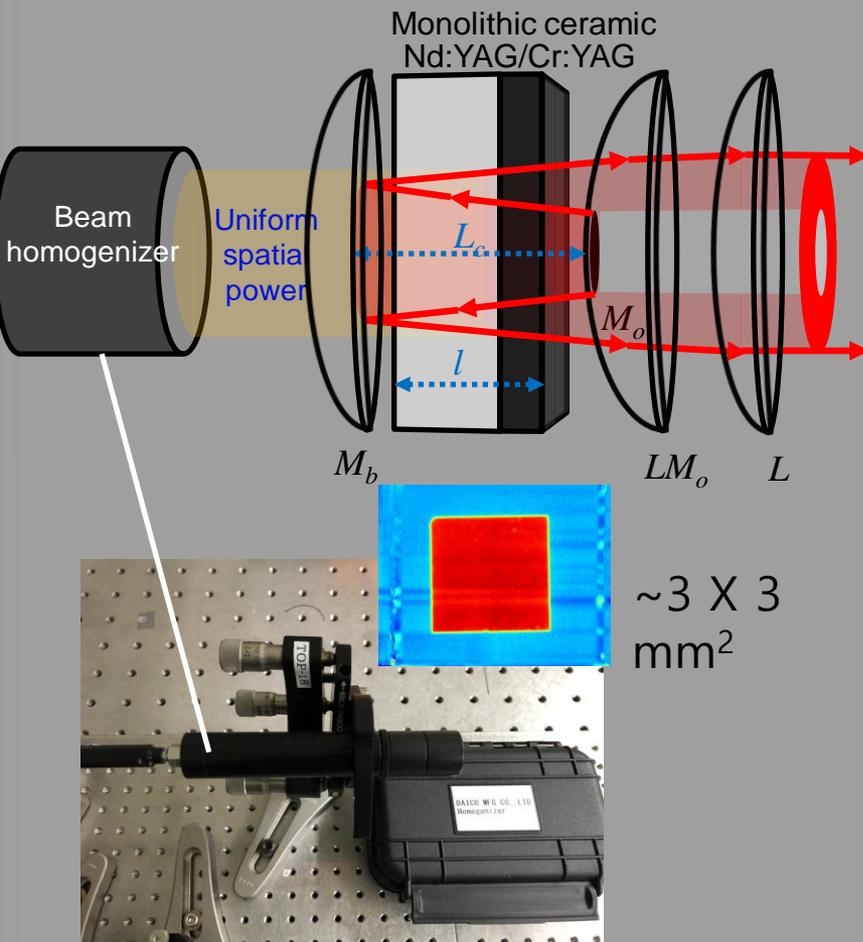
# Results of set-up II



- ▶ Doughnut beam pattern
- ▶ Pulse energy of 17 mJ @ 20 Hz
- ▶ Pulse width of 452 ps
- ▶ New record peak power of 37.6 MW

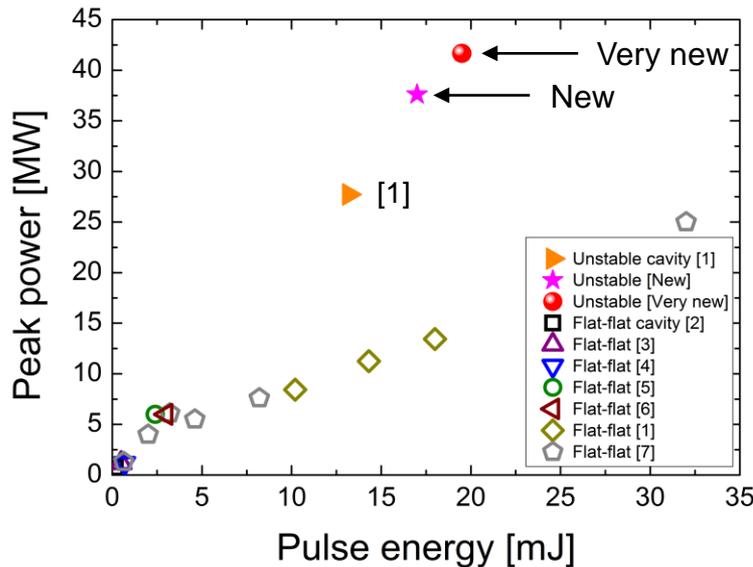
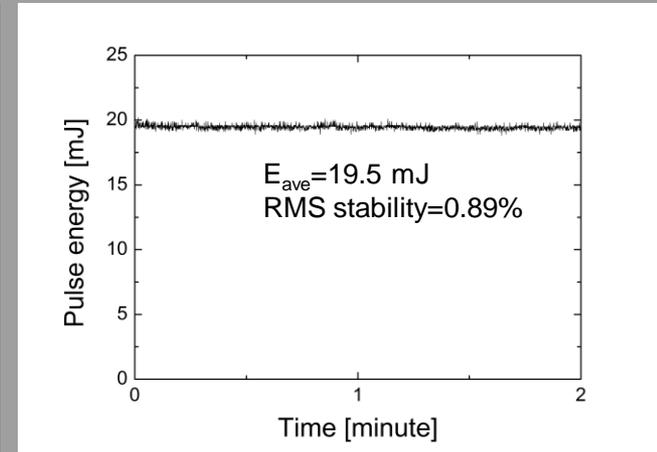
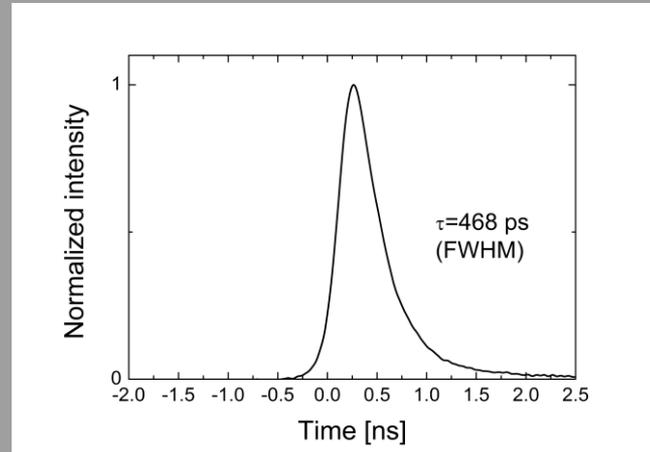
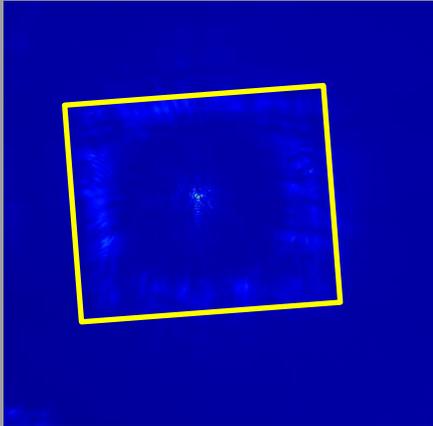
[1] H. H. Lim and T. Taira, Opt. Express **27**, 31307

# Experimental setup III : concave-convex cavity & uniform pump-power distribution



- ▶ 1.5 kW pump diode @ 808 nm, 20 Hz during <400  $\mu\text{s}$
- ▶ Uniform pump power distribution:  $\sim 3 \times 3 \text{ mm}^2$
- ▶ Concave back cavity mirror  $M_b$  with a radius of curvature of 250 mm
- ▶ A half inch plano-convex lens  $LM_0$  with a radius of curvature of 52 mm (for  $m$  of  $\sqrt{2}$  for the confocal cavity)
- ▶ Output coupler (OC)  $M_o$ , HR coated on the center part of  $LM_0$  in a spot diameter of 2 mm
- ▶ Collimation lens  $L$  with a focal length of 50~150 mm in case of the lens position

# Results of set-up III

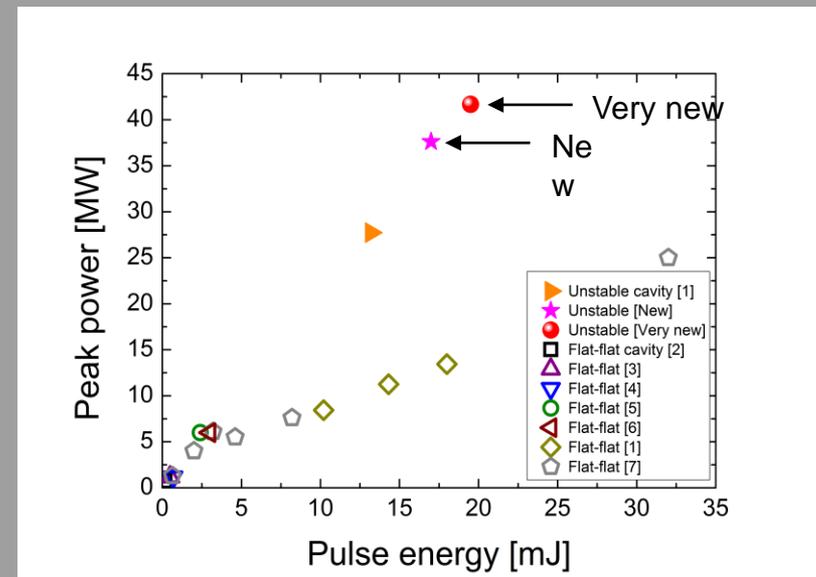
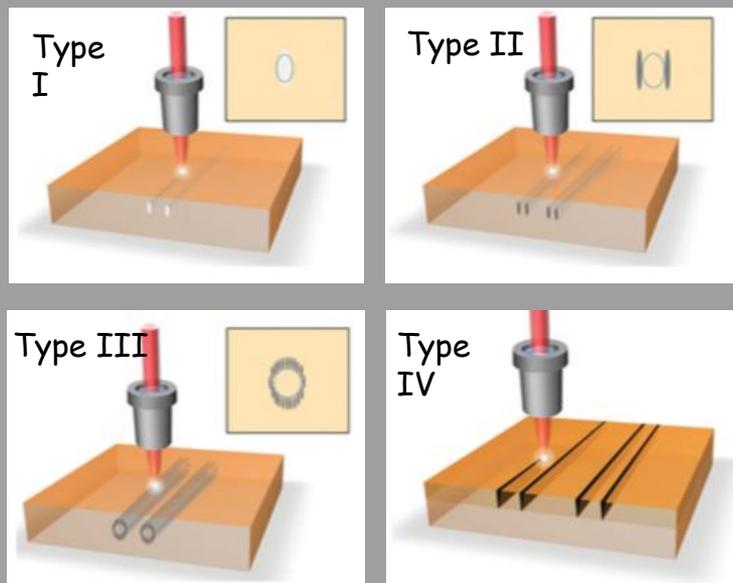


- ▶ Modified doughnut beam pattern
- ▶ Pulse energy of 19.5 mJ @ 20 Hz
- ▶ Pulse width of 452 ps
- ▶ New record peak power of 41.7 MW

[1] H. H. Lim and T. Taira, Opt. Express **27**, 31307

# Summary

- ◆ Overview of fs laser micromachined waveguides
- ◆ Record peak power unstable cavity microchip laser:
  - 41.7 MW, 19.5 mJ, 468 ps



# Future plan

- ◆ Laser writing system development (with Laser system Inc.).
- ◆ Test of unstable cavity MCL for laser writing (in laser and nonlinear materials such as Nd:YAG ceramics and crystals, LN, ...), which may be compared with a reference using a fs-laser from Prof. Sugimoto group ( $< 1$  mJ, 200 fs, 300 kHz) if possible.
- ◆ Further peak power and repetition rate scale of unstable cavity MCL using DFC chip.